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THE MODELING OF TEMPERATURE FIELDS IN VERTEBRA BONE AT STABILIZING VERTEBROPLASTY*

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Моделирование температурных полей в костной ткани позвонков при стабилизирующей вертебропластике

ABSTRACT

Purpose: To study the temperature fields caused by bone cement polymerization at the stabilizing vertebroplasty. To verify experimental data by thermohydraulic simulation. To modify program codes, applied in nuclear installations in order to adapt them to new object region.

Material and methods: Two groups of experiments involving the non-stationary temperature distribution measurements were done, namely, the cement polymerization: a) in the isolated cuvette; b) in a vertebra. For numerical modeling of experiments, the 3D non-stationary KANAL code applied in thermohydraulics of nuclear power plants is adapted.

Results: The satisfactory coherence of measured data and simulated ones is obtained for temperature distributions, the spatial and time-dependent as well. The most important is the closeness in experimental and simulating temperature maximum values at cement polymerization in a vertebra. The executed study grants the theoretical support of vertebroplasty in two aspects: a) by providing with the developed calculation techniques; b) by estimating the curative effect because of the bone tissue heating.

Ключевые слова: *spinal metastases, vertebroplasty, temperature fields, experimental and simulating modeling, numerical simulation, curative effect*

РЕФЕРАТ

Цель: Применительно к задачам стабилизирующей вертебропластики выполнить исследования температурных полей, обусловленных полимеризацией костного цемента. Верифицировать полученные результаты посредством термогидравлических расчетов. Модифицировать программные коды, используемые для расчета нестационарных температурных полей в ядерных установках, с целью их адаптации к новой предметной области.

Материал и методы: Выполнены две группы экспериментов по измерению нестационарного распределения температуры: а) при полимеризации цемента в изолированной кювете; б) при полимеризации цемента в позвонке. Для расчетного моделирования экспериментов адаптирован 3D нестационарный код КАНАЛ, применяемый в задачах теплогидравлики ядерных энергетических установок.

Результаты: Для обоих экспериментов достигнута удовлетворительная согласованность измеренных и рассчитанных температурных характеристик — как их пространственного, так и временного распределения. Особо существенной является близость экспериментальных и расчетных значений максимума температуры при полимеризации цемента в позвонке: типичные расхождения эксперимента и расчета не превышают 1–2 °С. Выполненное исследование обеспечивает теоретическую поддержку вертебропластики в двух аспектах: а) применением созданных расчетных технологий; б) оценкой степени терапевтического воздействия в результате нагрева костной ткани.

Key words: *метастазы в позвоночнике, вертебропластика, температурные поля, экспериментальное и расчетное моделирование, терапевтический эффект*

Introduction

Percutaneous vertebroplasty (PVP) as a way of vertebral structures stabilization was offered in 1987 by Galibert and Deramond [1, 2], and soon there were publications about its high efficiency for patients with metastatic defeat of vertebra bodies [3]. The first publications, in which the results of PVP were estimated, had very optimistic

character. In them there was reported about disappearance or essential reduction of a pain syndrome for 80–97 % of patients with the lytic and mixed metastasizes in a backbone [3–6]. For 15 % of patients the pain disappeared completely, for 55 % — it was considerably decreased, and for 30 % — the reduction of the pain intensity had moderate type. As result, the PVP technique began to be used widely as a method of pain suppression, at first at

* Данная статья на русском языке опубликована в журнале «Медицинская радиология и радиационная безопасность», Т. 60, № 4, С. 62–70.

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metastatic spinal compression fractures for patients with malignant new growths, and then and at the expressed pain syndrome against metastatic defeat of vertebrae when conservative therapy was inefficient [7–11].

Improvement of patients' life quality, in the main at the expense of the pain reduction and restoration of physical activity [12–18], was noted. In [19] it was claimed that for 75 % of patients the positive changes remained within 6 months. However, the subsequent estimates of PVP at metastatic defeats of a backbone in [20] showed that in 6 months only for about 40 % of the patients who have undergone vertebroplasty the need for anesthetics remained less, than before operation, and satisfactory quality of life remained. All these patients had isolated metastases of the minimum distribution in a vertebra of I, II, III types (K. Tomita [21] classification).

The extended tumors growth for them was not revealed due to the provided composite treatment. The patients with V, VI, and especially VII types of distribution had short-term efficiency of the PVP. In these cases, in 2 ÷ 6 months after vertebroplasty the expressed violations of the vertebra function were developed, quality of life was sharply decreased — it was caused, first of all, by fast increase of a pain syndrome. The metastatic zones tended to growth, settling down on the periphery of implanted bone cement, and they extended towards the vertebral channel, that also led to increase of a pain syndrome.

Summing up, it is possible to note that the positive effect of the stabilizing palliative vertebroplasty is shown only at rather early manifestations of metastatic growth in a vertebra. Thus, the metastatic zone should not overcome the terminate plate (i.e. vertebral arch), be accompanied with pathological fractures, be localized in 2–3 vertebrae or be of multiple distribution mode. In all cases of the stabilizing vertebroplasty the lack of the continued tumor growth can be provided only in the combination therapy [22].

It is supposed in [23, 24] that the necrosis of tumor tissue because of its heating as a result polymerization after cement implantation in the destructed zone is the reason of metastases relapse reduction after vertebroplasty. However, the experiments *ex vivo* [25, 26] as well as *in vivo* [27, 28] don't allow to draw an unambiguous conclusion that temperature in places of the maximum warming up of the bone tissue surrounding a cement kernel, reaches the values capable to cause a tumor tissue necrosis.

Analysis of the results of investigations performed formerly concerning temperature resistance of tumor cells testifies to:

- at 72 °C the necrosis of tumor cells arises immediately;
- at 60 °C — after 5 s exposure;
- at 55 °C — after 30 s exposure;
- at 50 °C — after 5 min exposure;
- at 47 °C — after 7 ÷ 13 min exposure;
- at 46 °C — after 20 ÷ 50 min exposure;
- at 45 °C — after 30 ÷ 60 min exposure;

- at 44 °C — after 45 ÷ 80 min exposure [29–31].

Apoptosis of cells occurs at lower temperatures, but at longer exposure [29, 30 and 32]. It is necessary up-to 4÷20 hours at 42 °C for complete destruction of various tumor cells [31]. Long-term action of insignificant temperature (less than 42 °C) is able to stimulate the proliferation of tumor cells [29–32].

Data published [29, 33 and 34] concerning the temperature characteristics of exothermic polymerization of quick-hardening bone cement on the base of polymethylmethacrylate, which is used at vertebroplasty, vary in wide limits and do not give the chance to define, whether there is enough temperature increase in the bone tissue surrounding the area of malignant growth, for the antitumor effect.

The simulation technique designing and its validation on experimental data which allows to prognosticate the level, depth and duration of a vertebra spongy bone substance warming up at exothermal polymerization of methyl acrylate (to get polymethylmethacrylate) at vertebroplasty was the goal of the work.

A series of experiments on the thermohydraulics characteristics study of bone cement hardening both in experimental cuvettes of various volume (the first stage of experiment) and in spongy tissue of the isolated vertebra (the second stage) is executed.

For the simulation of temperature time-dependence of bone warming up at implantation of bone cement, the calculation technology based on adaptation of the software applied in thermo-hydraulic calculations for nuclear power and another type plants was used.

Comparison of the temperature characteristics obtained at simulation with experimental data is carried out and the conclusion is drawn on possibility of reliable calculation the temperature level and duration of a bone tissue warming.

Experiments

At the first stage (experiment No. 1), measurements of the maximum temperature at bone cement polymerization in experimental cuvettes were carried out. Experiments at the first stage purposed to

- development of measurement technique;
- key parameters identification which influence the energy release under specific conditions of polymerization, which simulate real conditions at vertebroplasty.

Experimental cuvettes represented a set of aluminum cylinders (four pieces), each with two thermocouples. One of thermocouples was fixed on border of cement and a lateral cuvette wall, another — practically in the geometrical center of a cuvette (fig. 1).

Cuvette internal diameter was varied from 1.2 to 2.2 cm, and height of a volume filled with cement in a tube— from 1.5 to 1.8 cm. Cement with a density 1.34 g/cm³ and with heat conductivity coefficient 0.2 W/(m×K)



Fig. 1 Experimental tube with thermocouples (schematic)

was applied. Reference temperature of a mix before cement preparation was 21 °C.

To approach the real vertebroplasty conditions, cement at polymerization was isolated by means of a polyfoam (5 cm thick layer). In fig. 2 the polyfoam box photo, in which an experimental cuvette was placed, is submitted.

Temperature measurement at cement polymerization was carried out by means of the differential thermal analysis. The ZET 210 hardware module [35] with 16 inputs, connected to the computer, was basis of the measuring facility. As the sensing devices, standard normalizing amplifiers were used. The software of the ZET 210 module represents the complex integrated with the graphic interface; the one provides continuous signals registration.

Four series of experiments with four experiments in each were executed. During experiments, the bone cement Surgical Cement For Vertebroplasty “CementoFixx” (OptiMed) [36] was used. Cement was kneaded during 30 s and then it was injected into a cuvette by a syringe. This procedure takes 1 min — 1 min 20 s usually.

Results of measurements are presented in table 1 and in fig. 3. These data show that the temperature both on a cement kernel axis and on experimental cuvettes lateral surface nonlinearly depends on the volume of cement.

At the cuvette’s small volume, there is a great role of a cuvette surface size in temperature formation both on a surface, and in the cuvette center. With the growth of cuvette volume, the role of a cuvette surface in the convective heat exchange decreases, and the cuvette volume effects more and more, therefore the ratio t_a/t_l grows and changes with volume increase not so quickly as at the small cuvette volume.

Table 1

The temperature of cement (°C) on the cuvette axis (t_a) and on its lateral surface (t_l)

Tube No.	Cuvette dimensions*			t _l					t _a , Average value
	h, cm	d, cm	V, cm	Experiment No.				Average value	
				1	2	3	4		
1	1.6	1.2	1.8	92	96	93	96	94 ± 2	101 ± 3
2	1.5	1.6	3.0	104	107	105	106	105 ± 2	109 ± 1
3	1.8	1.8	4.6	107	109	108	109	108 ± 1	120 ± 3
4	1.7	2.2	6.5	110	112	113	113	111 ± 1	123 ± 2
Ambient air temperature, °C				20	19	21	21	20 ± 1	

* h — height; d — diameter; V — volume

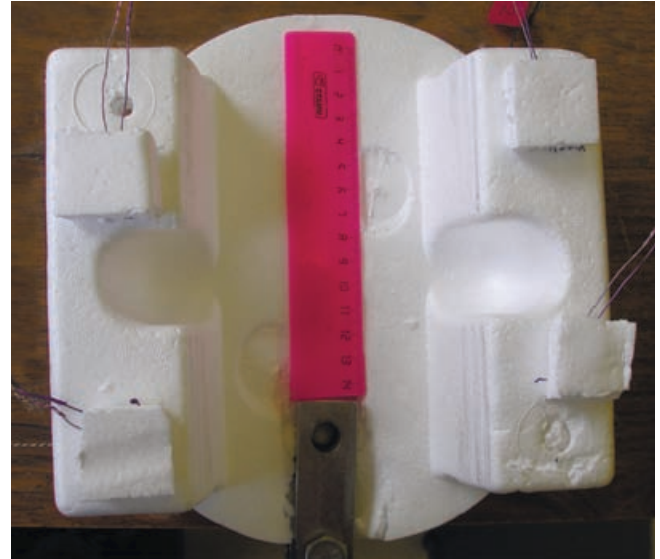


Fig. 2. Polyfoam isolating box for cuvette in the first experiment

At the second stage (experiment No. 2), time-dependence of temperature is obtained at polymerization of bone cement in vertebra cavity.

For measurements at the second stage the cylindrical cavity with $d \times h$ sizes = 1.8×1.8 cm, modeling a lytic metastasis, was formed in the center of the isolated vertebra. This cavity just before measurement was filled with bone cement by the same procedure as in the first experiment. Non-stationary temperature profile in the volume of a vertebral spongy bone was studied.

One of thermocouples in measurements was placed in the center of cement kernel (i.e. in the cylindrical cavity filled with cement) on its axis, other 15 thermocouples were settled down in a bone at various distances from a surface of cement contact with a bone. These thermocouples were located practically in the same plane on the middle of height of a vertebra (fig. 4).

The distance from a surface of a cement kernel is the most essential parameter that influences the sensor indications. The detector distance to a surface of the thermohydraulic characteristics rupture (i.e., to external

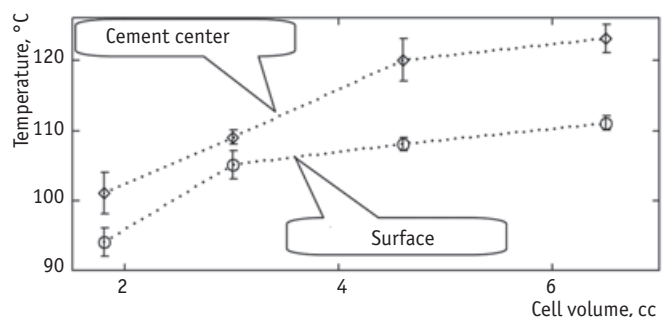


Fig. 3. The maximum temperature of bone cement on a surface and in the cuvette center as a function of its volume



Fig. 4. The vertebra photo with thermocouples (at the left); the 3D-reconstruction based on tomography scans (on the right)

border of a vertebra or to any other heterogeneity) is much less essential.

The vertebra prepared for experiment with the thermocouples installed in it was located in Petri dish filled with formalin isotonic 10 %-solution. Previously the bottom lamina of vertebral arch was removed for providing a uniform liquid elevation which prevents drying of bone tissue of a vertebra body. The specimen was incubated in the thermostat during not less than 3 h up to the uniform temperature in a spongy bone. The specified procedures are directed to (a) approach the experimental conditions to conditions at vertebroplasty, and (b) provide constancy of thermohydraulic conditions during experiment.

Process of polymerization was fixed by measurement instruments and checked visually on the display screen. At a temperature of air (38°C) the temperature of bone tissue was established at lower level ($32.6 \pm 0.1^{\circ}\text{C}$), that is explained by heat removal at liquid evaporation from a surface of a vertebra body.

The chosen detectors, the distance from which to a cement surface monotonously increases, are conditionally represented in fig. 5, and in fig. 6 the vertebra tomogram is submitted.

The time-dependant temperature in the center of a cement kernel, and also in bone tissue at different distance from a cement surface are given in fig. 7 for the chosen detectors. The characteristics of a spongy bone tissue warming up in experiment are provided in table 2: the maximum temperature in the detector location and an exposure time at a temperature above some value.

Properly both from measurements and from calculations, the effect of a hyperthermia is short-range (inside $2 \div 4$ mm from a surface of a cement kernel); therefore the influence of the actual geometry of a vertebra as well as metastatic «cavity» and its localization on temperature at polymerization is rather insignificant — no more than 10–20 % in a value. It follows that results of measurements possess sufficient generality and

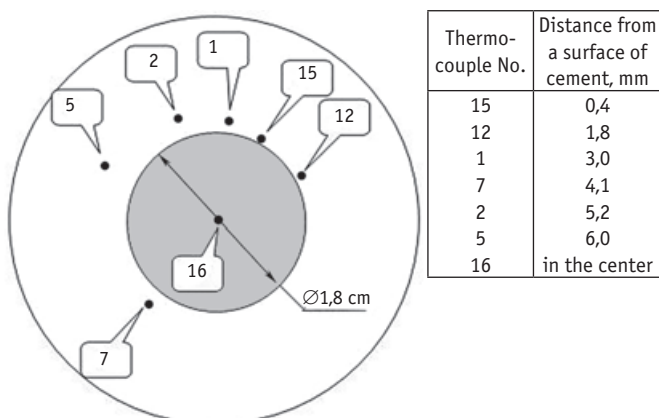


Fig. 5. The thermocouples location in a vertebra (conditionally; not in scale)

Table 2

The characteristics of the vertebra spongy bone's warming up

Distance from border of bone cement, mm	Maximum temperature, °C	Time (min ('), s (")), during which temperature is higher than the specified level			
		50 °C	47.5 °C	45 °C	42.5 °C
Center	118 ± 3				
Bone border	80 ± 3	6'	6'	7'	8'30"
0.4	58 ± 3	3'	4'	6'	7'30"
1.8	52 ± 1.1	1'30"	3'	4'30"	6'30"
2.5	50 ± 0.8	30"	2'30"	3'20"	6'
3.0	$46. \pm 0.3$	—	—	2'30"	5'
3.5	45 ± 0.3	—	—	< 30"	4'
4.1	41.5 ± 0.2	—	—	—	—

are applicable for the wide range of the geometrical characteristics, which are realizing at vertebroplasty.

Simulation

Computation of 2D non-stationary temperature field in the cuvettes was carried out by means of the KANAL code [37] intended for non-stationary thermohydraulic calculations for coolant systems of nuclear reactors. At calculation models design the code was adapted to provide heat generation and heat transfer in spongy bone tissue [38].

Two-dimensional non-stationary calculation of temperature in a vertebra with the cylindrical cement-filled cavity was executed. The data illustrating high consistency degree of temperature values shown in fig. 8, 9 were obtained:

- in experiment No. 1 for heat-insulated cuvette of 4.6 cm³ (fig.8, experimental curve);
- in computational simulation of the experiment No. 1 (fig. 8, calculated curve);
- in experiment No. 2 simulating lytic metastasis cavity of 4.6 cm³ surrounded with spongy bone tissue at a temperature of $32.6 \pm 0.1^\circ\text{C}$ (fig. 9, experimental curve);
- in computational simulation of the experiment No. 2 (fig. 9, calculated curve).

The basic data accepted for calculation of temperature distribution in bone tissue are given in table 3.

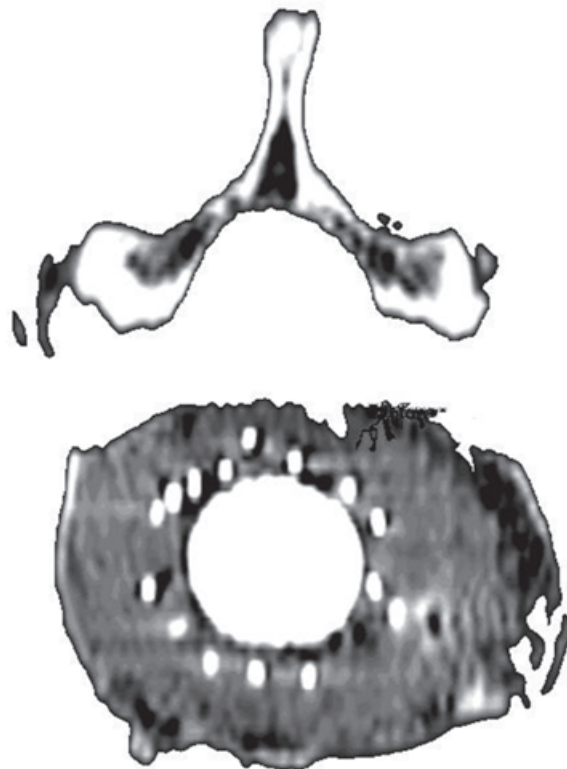


Fig. 6. The vertebra tomogram with the installed thermocouples

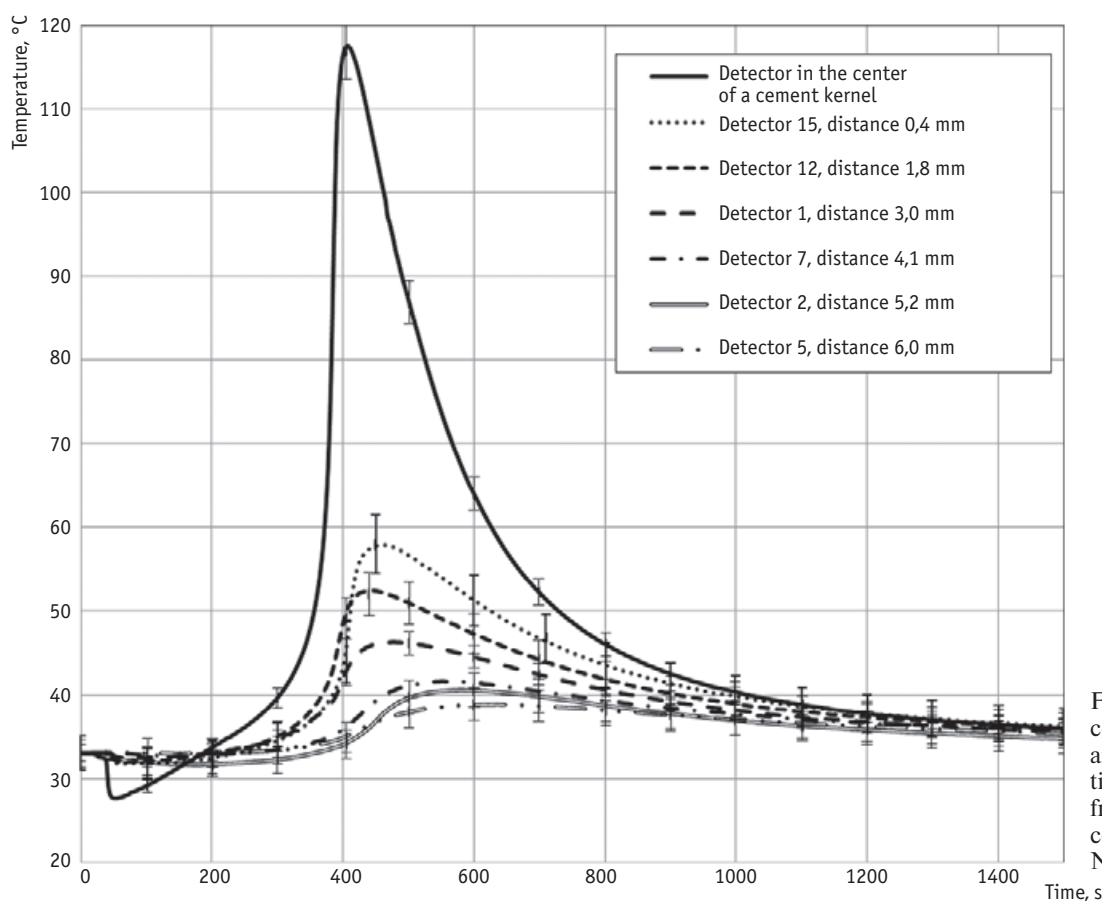


Fig. 7. Temperature in the center of cement “kernel” and in vertebra bone tissue at various distance from a surface of bone cement (the experiment No. 2)

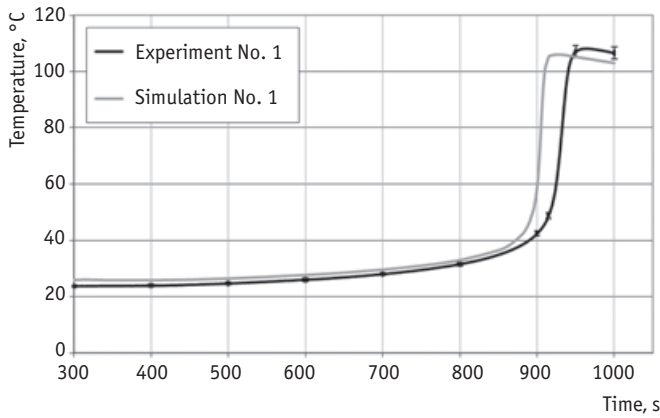


Fig. 8. Temperature time dependence on an internal surface of a cuvette wall (experiment and calculation No. 1)

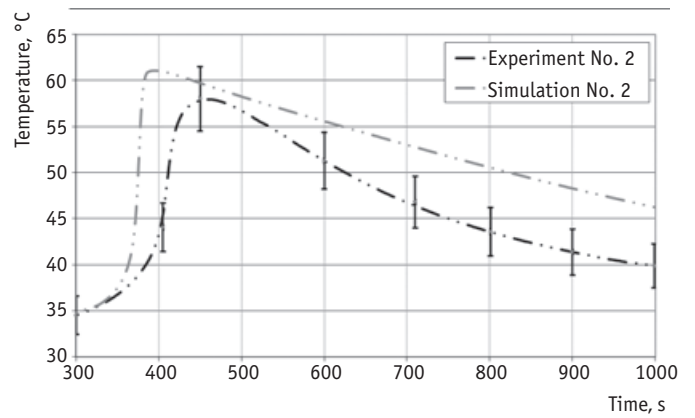


Fig. 9. Temperature time dependence on lateral surface of a cement kernel (experiment and calculation No. 2)

Table 3

Input data for 2D non-stationary calculation of temperature in a vertebra with a cylindrical cavity

Diameter and height of the cement-filled cavity, mm	18; 18
Diameter and height of the vertebra, mm	36; 24
Density of bone tissue of a vertebra, kg/m ³	1180
Specific heat of bone tissue, J/(kg×K)	2270
Heat conductivity of bone tissue, W/(m×K)	0.31
Starting temperature of water, cement, vertebra, °C	32.6; 27.5; 32.6

Discussion

The obtained results allowed to apply the developed technique to simulate a warming up of bone tissue on interface with cement and on various distances from it. Comparison of calculated results with the data obtained in a series of experiments with bone cement-filled cavity of the same volume (fig. 10) shows high degree coherence of simulated and experimental data. It allows to draw a conclusion on possibility of thermal impact prediction on surrounding cells and tissues at bone cement implantation in a metastatic cavity of known volume.

From Fig. 7 and Table 2 follows that the temperature necrosis of all tumor cells can arise at distance no more than 0.4 mm from border of bone cement where temperature remains above 50 ± 3 °C during 3 min reaching maximum value 58 °C. At distance from 0.4 to 1 mm there is a mass death of tumor cells, however their total elimination cannot be reached. At distance from 1 to 2.5 mm profound dystrophic changes of tumor cells and considerable delays of their growth are provided. At distance of 2.5 mm and more, the death of tumor cells caused by thermal influence is not predicted; the apoptosis activation is prognosticated. On the basis of numerous studies of a tumor cells temperature radiosensitivity (see, for example, [39]), it is possible to expect that at a distance up to 7 mm from

border of bone cement the radiosensitivity of tumor cells increases.

There is a diagram (fig. 11) of temperature effects on tumor cells in bone tissue of the vertebra surrounded with biological tissue. Borders of effects were defined based on data [29–31] that associate duration of influence and effect from this influence. As levels of temperature and the time exposure necessary for destruction of tumor cells, the following values were accepted:

- at 72 °C the necrosis arises instantly;
- at 60 °C the necrosis arises after 5 s exposure;
- at 55 °C the necrosis arises after 30 s exposure;
- at 50 °C the necrosis arises after 5 min exposure;
- at 47 °C the necrosis arises after 10 min exposure.

In fig. 11, all possible effects of thermal influence are presented at temperatures reached in experiment. These effects are shown depending on the volume V of bone cement and distance r from a surface of bone cement. Three effects can be observed: necrosis, apoptosis

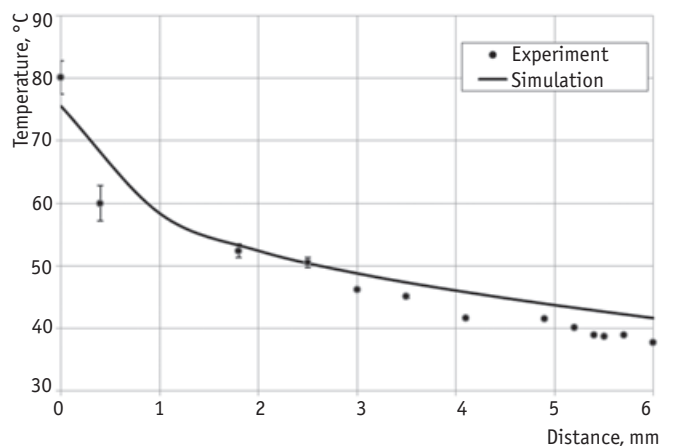


Fig. 10. Temperature maximum distribution in bone tissue of a vertebra body at different distance from a surface of bone cement

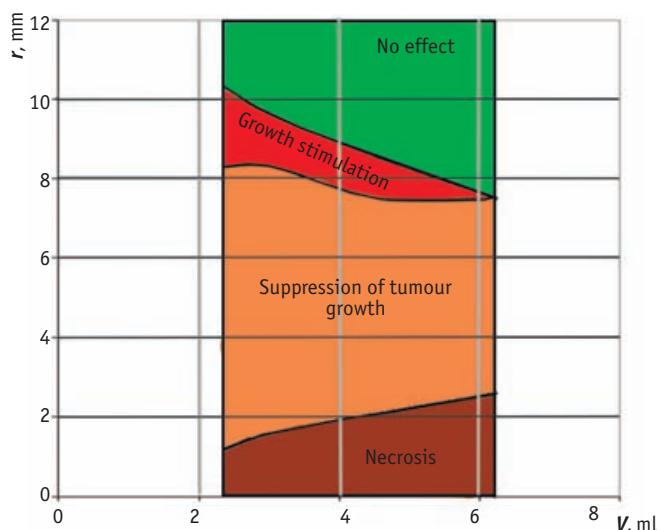


Fig. 11. Possible effects in vertebra bone tissue depending on the volume of bone cement and distance from a contact surface of cement and bone tissue

activation with suppression of growth of tumor cells and stimulation of their growth.

The temperature 40 °C at time exposure no more than 100 s is chosen as the temperature at which thermal influence does not render any effect. Tumor cells growth stimulation is possible in the range of temperature 40–41.5 °C and in any time exposure [29–32].

The necrosis of tumor cells, even at implantation more than 6 cm³ of bone cement in a cavity of the lytic or mixed metastasis, doesn't reach border of infiltrative growth of a tumor. Areas of apoptosis stimulation, suppression of tumor growth and radiosensibilization of tumor cells are significantly more. Stimulation of tumor growth (at temperatures 40–41.5 °C) arises at implantation of small cement volume when the area of suppression of malignant growth does not extend to an arch plate of a vertebra body or when the soft-tissue component of metastatic growth takes place. At the sufficient volume of a cement implanted in a lytic cavity of a metastasis, the temperature radiosensibilization of tumor cells is reached practically in all volume of a vertebra body.

Conclusion

1. Experimental researches of non-stationary temperature fields have been conducted at polymerization of bone cement in a vertebra at stabilizing vertebroplasty.
2. The experimental model of a local hyperthermia in the area of tumor growth in spongy tissue of a vertebra body is developed.
3. The calculation technology and the software allowing to predict (with a sufficient accuracy for practical application) a warming up of bone tissue at different

distances from border of bone cement is developed and approved.

4. It is shown that at implantation of high-temperature bone cement into a cavity of a lytic metastasis, the temperature more than 70 °C is reached on border between cement surface and bone tissue.
5. Results obtained can be used at dosimetric planning of the external-beam or intervention radionuclide therapy carried out after the PVP operation of vertebra bone metastases.

Acknowledgment

Authors thank Professor Vladimir A. Stepanov, the Head of the Department of Material Science in Institute of Nuclear Power Engineering, for fruitful discussion and the invaluable help when performing the experimental research.

REFERENCES

1. Galibert P., Deramond H., Rosat P., Le Gars D. Note préliminaire sur le traitement des angiomes vertébraux par vertébroplastie acrylique percutanée. // *Neuro chirurgie*, 1987, **33**, P. 166–168.
2. Deramond H., Depriester C., Galibert P., Le Gars D. Percutaneous vertebroplasty with polymethyl methacrylate. Technique, indications, and results. // *Radiol. Clin. North Amer.*, 1998, **36**, P. 533–546.
3. Kaemmerlen P., Thiesse P., Jonas P. et al. Percutaneous injection of orthopaedic cement in metastatic vertebral lesions. // *N. Engl. J. Med.*, 1989, **321**, No. 2, P. 121–132.
4. Aliev M., Dolgushin B., Teplyakov V., Valiev A. Transcutaneous vertebroplasty in combined treatment of patients with tumoral lesions of the spine. // *EMSOS*, 2003, abs A-044, P. 72.
5. Aliev M., Teplyakov V., Karpenko V., Valiev A. Vertebroplasty as a choice of treatment of painful syndrome in patients with tumoral lesions of the spine. // *EMSOS*, 2004, abs 28, P. 5.
6. Cortet B., Cotton B., Boutry N. et al. Percutaneous vertebroplasty in patients with osteolytic metastases or multiple myeloma. // *Rev. Rheum. Engl. Ed.*, 1997, **64**, No. 3, P. 177–183.
7. Валиев М.А., Мусаев Э.Р., Тепляков В.В. и соавт. Чрескожная вертебропластика в онкологии. Под ред. М.Д. Алиева, Б.И. Долгушина. — М.: ИНФРА-М, 2010, 71 с.
8. Алиев М.Д., Соколовский В.А. Высокотехнологичное лечение в онкоортопедии. — М., 2008, 24 с.
9. Пташников Д.А., Усиков В.Д., Корытова Л.И. и соавт. Pathological fractures of spine caused by tumor: diagnostics and treatment tactic. // In: "First International Scientific Distance Congress on Spine and Spinal Cord Surgery "InterSpine — 2004", Saint-Petersburg, Russia, September, 2004, P. 36–38.
10. Кустов А.В., Жаринов Г.М., Рудь С.Д. и соавт. Изучение эффективности пункционной вертебропластики и лучевой терапии в лечении агрессивных ге-

- мангиом позвоночника. // Мед. акад. журнал, 2008, № 4, С. 101–114.
11. Джинджихадзе Р.С., Лазарев В.А., Горожанин А.В. и соавт. Перкутанная вертебропластика. // Нейрохирургия, 2005, № 1, С. 36–41.
 12. Diamond T.H., Champion B., Clark W.A. Management of acute osteoporotic vertebral fractures: a nonrandomized trial comparing percutaneous vertebroplasty with conservative therapy. // Amer. J. Med., 2003, **114**, No. 4, P. 257–265.
 13. Perez-Higueras A., Alvarez L., Rossi R.E. et al. Percutaneous vertebroplasty: long-term clinical and radiological outcome. // Neuroradiology, 2002, **44**, No. 11, P. 950–954.
 14. Martin J.B., Wetzel S.G., Seium Y. et al. Percutaneous vertebroplasty in metastatic disease: transpedicular access and treatment of lysed pedicles—initial experience. // Radiology, 2003, **229**, No. 2, P. 593–597.
 15. Stricker K., Orlor R., Yen K. et al. Severe hypercapnia due to pulmonary embolism of polymethyl methacrylate during vertebroplasty. // Anesth. Analg., 2004, **98**, No. 4, P. 1184–1186.
 16. Choe Du H., Marom E.M., Ahrar K. et al. Pulmonary embolism of polymethyl methacrylate during percutaneous vertebroplasty and kyphoplasty. // AJR Amer. J. Roentgenol., 2004, **183**, No. 4, P. 1097–1102.
 17. Yoo K.Y., Jeong S.W., Yoon W., Lee J. Acute respiratory distress syndrome associated with pulmonary cement embolism following percutaneous vertebroplasty with polymethyl methacrylate. // Spine, 2004, **29**, No. 14, P. 294–297.
 18. Nussbaum D.A., Gailloud P., Murphy K. A review of complications associated with vertebroplasty and kyphoplasty as reported to the Food and Drug Administration medical device related web site. // J. Vasc. Interv. Radiol., 2004, **15**, No. 11, P. 1185–1192.
 19. Cortet B., Cotton B., Boutry N. et al. Percutaneous vertebroplasty in patients with osteolytic metastases or multiple myeloma. // Rev. Rheum. Engl. Ed., 1997, **64**, No. 3, P. 177–183.
 20. Мануковский В.А. Вертебропластика в лечении патологии позвоночника (клинико-экспериментальное исследование). — СПб.: Автореферат дисс. докт. мед. наук, 2009, 45 с.
 21. Tomita K., Kawahara N., Kobayashi T. et al. Surgical strategy for spinal metastases. // Spine, 2001, **26**, No. 3, P. 298–330.
 22. Kaneko T. S., Sehgal V., Skinner H.B. et al. Radioactive bone cement for the treatment of spinal metastases: a dosimetric analysis of simulated clinical scenarios. // Phys. Med. Biol., 2012, **57**, P. 4387–4401.
 23. San Millan R.D., Burkhardt K., Jean B. et al. Pathology findings with acrylic implants. // Bone, 1999, **25**, No. 2, P. 85–90.
 24. Wetzel S.G., Martin J.B., Somon T. et al. Painful osteolytic metastasis of the atlas: treatment with percutaneous vertebroplasty. // Spine, 2002, **27**, No. 22, P. 493–495.
 25. Deramond H., Wright N.T., Belkoff S.M. Temperature elevation caused by bone cement polymerization during vertebroplasty. // Bone, 1999, **25**, No. 2, P. 17–21.
 26. Belkoff S.M., Molloy S. Temperature measurement during polymerization of polymethylmethacrylate cement used for vertebroplasty. // Spine, 2003, **28**, No. 14, P. 1555–1559.
 27. Verlaan J.J., Oner F.C., Verbout A.J. et al. Temperature elevation after vertebroplasty with polymethylmethacrylate in the goat spine. // J. Biomed. Mater. Res. B: Appl. Biomater., 2003, **67**, No. 1, P. 581–585.
 28. Anselmetti G., Manca A., Kanika Kh. et al. Temperature measurement during polymerization of bone cement in percutaneous vertebroplasty: An in vivo study in humans. // Cardiovasc. Intervent. Radiol., 2009, **32**, P. 491–498.
 29. Фрадкин С.З. Современное состояние гипертермической онкологии и тенденции ее развития. // Мед. новости, 2004, № 3, С. 3–8.
 30. Li C., Chien S., Branemark P.I. Heat shock-induced necrosis and apoptosis in osteoblasts. // J. Orthop. Res., 1999, **17**, No. 6, P. 891–899.
 31. Eriksson R.A., Albrektsson T., Magnusson B. Assessment of bone viability after heat trauma. A histological, histochemical and vital microscopic study in the rabbit. // Scand. J. Plast. Reconstr. Surg., 1984, **18**, No. 3, P. 261–268.
 32. Александров Н.Н., Савченко Н.Е., Фрадкин С.З. и соавт. Применение гипертермии и гипергликемии при лечении злокачественных опухолей. — М.: Медицина, 1980, 256 с.
 33. Li S., Kotha S., Huang C.H. et al. Finite element thermal analysis of bone cement for joint replacements. // J. Biomech. Eng., 2003, **125**, No. 3, P. 315–322.
 34. Po-Liang Lai, Ching-Lung Tai, Lih-Huei Chen et al. Cement leakage causes potential thermal injury in vertebroplasty. 2011. <http://www.biomedcentral.com/1471-2474/12/116>.
 35. Модуль АЦП/ЦАП ZET 210. http://www.zetlab.ru/catalog/ACP/ZET_210/
 36. CementoFixx-R Hauptmerkmale Opti Med. Global Care. Instructions for use surgical cement for vertebroplasty sterile, radiopaque. 2004. 120 pp. http://www.opti-med.de/uploads/tx_vaproducts/CementoFixx-R-M-L_03-2013.pdf.
 37. Канал. Теплогидравлический код. Описание численной схемы кода КАНАЛ. Отчет о НИР. Том 7. — Обнинск: ЭНИМЦ МС, 2008, 95 с.
 38. Вознесенский Н.К., Богданов Н.В., Дорохович С.Л. и соавт. Моделирование гипертермии при стабилизирующей вертебропластике. // Ядерная энергетика, 2013, № 1, С. 37–48.
 39. Overgaard J. The current and potential role of hyperthermia in radiotherapy. // Int. J. Radiat. Oncol. Biol. Phys., 1989, **16**, P. 535–549.

Поступила: 01.10.2014

Принята к публикации: 27.05.2015